

Partie 1

Q1a  $M_t = M_v + M_c$

AN -  $M_t = 57000 \text{ kg}$

(0,5)

Q1b

$a < \vec{FG} \cdot \vec{x}_1 < b$

$M_t \vec{FG} = M_v \vec{FG}_v + M_c \vec{FG}_c$

$\vec{FG} \cdot \vec{x}_1 = \frac{M_v}{M_t} c + \frac{M_c}{M_t} d$

$(a - \frac{M_v}{M_t} c) \frac{M_t}{M_c} < d < (b - \frac{M_v}{M_t} c) \frac{M_t}{M_c}$  (1)

AN :  $-0,12 < d < 1,78 \text{ m}$  (0,5)

Partie 2

Q2a. 2 plans de symétrie + passant par  $Axyz \Rightarrow D = E = F = 0$   
 solide de révolution /  $Az_1 \Rightarrow A = B$  (1)

$J_{2x} = J_{2y}$

Q2.b

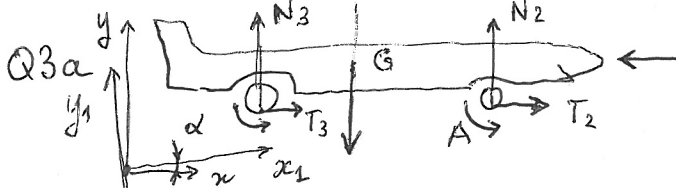
$[I_{A, b_1(z)}] = \begin{pmatrix} 2(J_{2x} + m_2 e^2) & 0 & 0 \\ 0 & 2(J_{2y} + m_2 e^2) & 0 \\ 0 & 0 & 2J_{2z} \end{pmatrix}$

$A(z) = B(z)$

(1,5)

Partie 3

$\dot{x} = v \quad \dot{\theta}_2 = \dot{\theta}_3 = \omega \vec{e}$



Q3a

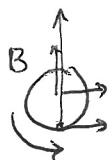
$\Sigma \vec{F}_{ext} \rightarrow \vec{\varepsilon} = \vec{0}$

BAMext  $\left\{ \begin{array}{l} \text{pes} \rightarrow 1 \quad -Mg \vec{y} \\ \text{vat} \rightarrow 1 \quad -k_1 (\dot{x} - v_0)^2 \vec{x}_1 \\ \text{sol} \rightarrow 2 \quad \left\{ \begin{array}{l} T_i \\ N_i \end{array} \right\} \left\{ \begin{array}{l} 0 \\ 0 \end{array} \right\} \\ \text{sol} \rightarrow 3 \quad \left\{ \begin{array}{l} N_i \\ 0 \end{array} \right\} \left\{ \begin{array}{l} 0 \\ k_i N_i \end{array} \right\} I_i \end{array} \right.$

$\left\{ \begin{array}{l} T_3 + T_2 - k_1 (\dot{x} - v_0)^2 - Mg \sin \alpha = 0 \\ N_3 + N_2 - Mg \cos \alpha = 0 \end{array} \right\}$  (0,5)

$\left\{ \begin{array}{l} k_1 N_3 + k_2 N_2 - (l+L) N_3 + Mg(\cos \alpha \cdot L + h \sin \alpha) = 0 \\ + k_1 (\dot{x} - v_0)^2 \cdot h \end{array} \right\}$  (0,5)

on isole (3)



$\Sigma \vec{M}_{B \text{ ext} \rightarrow 3} = \vec{0}$

$R_3 \cdot T_3 + k_3 N_3 = 0$  (0,5)

Q3b existence du contact  $N_2 > 0$   $N_3 > 0$

non glissement  $|T_2| < f N_2$   $|T_3| < f N_3$

(0,5)

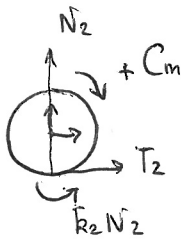
Q3c

$$\textcircled{1} \quad N_2 = Mg \cos \alpha - N_3 = Mg \cos \alpha - \left\{ \frac{Mg(L \cos \alpha + h \sin \alpha)}{(L+l)} + k_1(\dot{x} - v_0)^2 \cdot \frac{h}{(L+l)} \right\}$$

$$\textcircled{1} \quad T_2 = Mg \sin \alpha + k_1(\dot{x} - v_0)^2 + \frac{k_3}{R_3} \left\{ \frac{Mg(L \cos \alpha + h \sin \alpha)}{(L+l)} + k_1(\dot{x} - v_0)^2 \frac{h}{(L+l)} \right\}$$

$$f \geq \frac{T_2}{N_2}$$

Q3d on isole (2)



(1)

$$-C_m + T_2 \cdot R + k_2 N_2 = 0$$

$$C_m = R \cdot T_2 + k_2 N_2$$

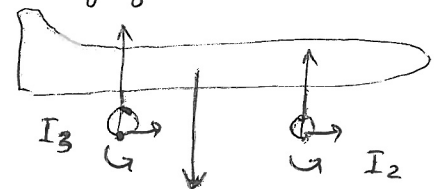
Q3e le calcul de  $T_2$  et  $N_2$  donne  $\frac{T_2}{N_2} = 0,62$  ( $< 0,7$ ) (1)

Partie 4 ( $\alpha = 0$   $k_1 = 0$ )

Q4.a RSG  $\dot{x} + R_2 \dot{\theta}_2 = 0$   $\dot{x} + R_3 \dot{\theta}_3 = 0$  (1)

Q4.b  $\sum \vec{F}_{ext} = R d(\varepsilon/R_g) = M \cdot \ddot{x} \vec{x}_1$  ( $M_2$  et  $M_3$  négligés)

(0,5) 
$$\begin{cases} T_2 + T_3 = M \ddot{x} \\ N_2 + N_3 - Mg = 0 \end{cases}$$



$$\sum \vec{M}_{I_2 \text{ ext } \rightarrow \varepsilon} = \vec{\delta}_{I_2}(\varepsilon/R_g)$$

$$\vec{\delta}_{I_2, 1/R_3} = -M \ddot{x} \cdot h$$

$$k_2 N_2 + MgL - N_3(L+l)$$

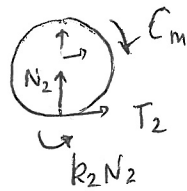
$$\vec{\delta}_{I_2, 2/R_3} = J_2 \ddot{\theta}_2 + 0$$

$$\vec{\delta}_{I_2, 3/R_3} = J_3 \ddot{\theta}_3 + 0$$

$$k_3 N_3 + k_2 N_2 + MgL - N_3(L+l) = J_2 \ddot{\theta}_2 + J_3 \ddot{\theta}_3 - Mh \ddot{x}$$

(1)

on side (2)



$$T_2 R_2 + k_2 N_2 - C_m = J_2 \ddot{\theta}_2$$

(1)

on side (3) par analogie

$$T_3 R_3 + k_3 N_3 = J_3 \ddot{\theta}_3$$

Q4c

$$|T_2| \leq F N_2$$

(0,5)

Q4d

$$N_3(L+l) = MgL + \underbrace{\left[ Mh + \left( \frac{J_2}{R_2} + \frac{J_3}{R_3} \right) \right]}_A \ddot{x} - k_2 N_2 \rightarrow N_3$$

$$N_3 = \frac{MgL + A \ddot{x}}{(L+l)} - \frac{k_2 N_2}{(L+l)}$$

$$N_2 = Mg - \frac{MgL}{(L+l)} - \frac{A \ddot{x}}{(L+l)} = \frac{Mg l}{(L+l)} - \frac{A \ddot{x}}{(L+l)} \quad (1)$$

$$N_2 > 0 \quad \ddot{x} \ll \frac{Mg l}{A} \quad (1)$$

$$T_3 = -\frac{k_3}{R_3} N_3 \approx \frac{J_3}{R_3^2} \ddot{x}$$

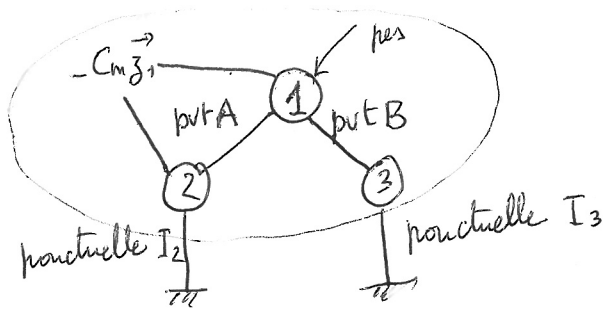
$$T_2 = M \ddot{x} - T_3 = M \ddot{x} + \frac{k_3}{R_3} N_3 + \frac{J_3}{R_3^2} \ddot{x}$$

$$T_2 = \left[ M + \frac{J_3}{R_3^2} + \frac{k_3}{R_3} \frac{A}{(L+l)} \right] \ddot{x} + \frac{k_3}{R_3} \frac{Mg l}{(L+l)} \quad (1)$$

$$\frac{T_2}{N_2} \leq F \quad (1)$$

on trouve  $\frac{T_2}{N_2} = 0,65 \quad (1,5)$

# Partie 5



①

on isole l' $\Sigma$

$$P_{ext} \rightarrow \Sigma, R_g + P_{int} = \left( \frac{dEc(\Sigma/R_g)}{dt} \right) / R_g$$

-  $R_{Sg}$  en  $I_2$  et  $I_3$

il reste  $k_2 N_2 \cdot \dot{\theta}_2 + k_3 N_3 \dot{\theta}_3$

~~pas de~~  $\ominus$

$$-C_m \dot{\theta}_2 = \frac{C_m \dot{x}}{R_2} \quad (0,5)$$

$$Ec(\Sigma) = Ec(1) + Ec(2) + Ec(3)$$

$$= \frac{1}{2} M \dot{x}^2 + \frac{1}{2} J_2 \dot{\theta}_2^2 + \frac{1}{2} J_3 \dot{\theta}_3^2 \quad (0,5)$$

$$C_m \frac{\dot{x}}{R_2} = M \dot{x} \ddot{x} + \frac{J_2}{R_2^2} \dot{x} \ddot{x} + \frac{J_3}{R_3^2} \dot{x} \ddot{x} + Mg \sin \alpha \dot{x} + k_1 (\dot{x} - v_0)^2 \dot{x}$$

en négligeant  $k_2$  et  $k_3$

- perte  $- Mg \sin \alpha \cdot \dot{x}$

- ari  $- k_1 (\dot{x} - v_0)^2 \dot{x}$

$$C_m = R_2 \left\{ \left( M + \frac{J_2}{R_2^2} + \frac{J_3}{R_3^2} \right) \dot{x} + Mg \sin \alpha + k_1 (\dot{x} - v_0)^2 \right\}$$

en négligeant  $k_2$  et  $k_3$

①