

$$Q1: \vec{\Omega}_{1/0} = \dot{\psi} \vec{z}_1; \quad \vec{\Omega}_{2/0} = \dot{\psi} \vec{z}_1 + \dot{\theta}_2 \vec{y}_1 = \begin{pmatrix} -\dot{\psi} \sin \theta_2 \\ \dot{\theta}_2 \\ \frac{1}{2} \dot{\psi} \cos \theta_2 \end{pmatrix}$$

$$Q2: \vec{V}_{G_2/0} = \begin{pmatrix} b_2 \dot{\theta}_2 \\ (a_2 + b_2 \sin \theta_2) \dot{\psi} \\ 0 \end{pmatrix}$$

Q3: On isole S_2 ; on applique le th. du mt dynamique en O_2 en projection sur \vec{y}_1

$$Q4: \vec{\sigma}_{O_2/0} \cdot \vec{y}_1 = \vec{J}_{O_2}(\text{rot}_2) \vec{y}_1 + C_{m_2}$$

$$B_2 \ddot{\theta}_2 = C_{m_2} + b_2 M_2 g \sin \theta_2$$

$$\text{soit } C_{m_2} = B_2 \ddot{\theta}_2 - b_2 \sin \theta_2 M_2 g$$

$$C_{m_3} = B_3 \ddot{\theta}_3 - b_3 M_3 g \sin \theta_3$$

$$Q5: \vec{a}_{G_2/0} = \begin{pmatrix} -\omega^2 (a_2 + b_2 \sin \theta_2) \cos \theta_2 + b_2 \ddot{\theta}_2 \\ 2b_2 \omega \dot{\theta}_2 \cos \theta_2 \\ -(a_2 + b_2 \sin \theta_2) \omega^2 \sin \theta_2 - b_2 \dot{\theta}_2^2 \end{pmatrix}$$

$$Q6: \vec{\sigma}_{O_1/S_1/0} = I_A \omega \vec{z}_1; \quad \vec{\sigma}_{O_1/S_1/0} = \vec{0}$$

Q7:

$$\vec{a}_{O_2/0} = \begin{pmatrix} -(A_2 \sin \theta_2 + M_2 a_2 b_2) \omega \\ B_2 \ddot{\theta}_2 \\ C_2 \omega \cos \theta_2 \end{pmatrix}$$

O_2 n'est pas un pt fixe.

Q8:

$$\vec{\sigma}_{O_2/S_2/0} = \begin{pmatrix} (C_2 - A_2 - B_2) \cos \theta_2 \omega \dot{\theta}_2 \\ B_2 \ddot{\theta}_2 + [(C_2 - A_2) \sin \theta_2 - M_2 a_2 b_2] \omega^2 \cos \theta_2 \\ (A_2 - C_2 - B_2) \sin \theta_2 \omega \dot{\theta}_2 \end{pmatrix}$$

$$Q9: \text{Calcul en } O_1 \text{ et projection sur } R_1 \text{ avec } b_2 = 0 \text{ on obtient } O_1 \vec{\sigma}_2 \wedge M_2 \vec{a}_{G_2/0} = \vec{0}$$

$$\vec{\sigma}_{O_1 S_2 / O} = \begin{cases} (I_2 \cos^2 \theta_2 + J_2 \sin^2 \theta_2) \omega \dot{\theta}_2 = D_1 & \text{avec } I_2 = C_2 - A_2 - B_2 \\ B_2 \ddot{\theta}_2 + (C_2 - A_2) \sin \theta_2 \cos \theta_2 \omega^2 = D_2 & J_2 = A_2 - C_2 - B_2 \\ (J_2 - I_2) \cos \theta_2 \sin \theta_2 \omega \dot{\theta}_2 = D_3 \end{cases}$$

Q.10: On isole S_2 et on écrit $\vec{\sigma}_{O_2, 2/0} \cdot \vec{y}_1' = \vec{H}_{O_2}(\text{Poids de } S_2) \cdot \vec{y}_1' + C_{m_2}$

On isole S_3 $\vec{\sigma}_{O_3, 3/0} \cdot \vec{y}_1' = \vec{H}_{O_3}(\text{Poids de } S_3) \cdot \vec{y}_1' + C_{m_3}$

On isole $S_1 + S_2 + S_3$ et on écrit.

$$\left(\vec{\sigma}_{O_1, 2/0} + \vec{\sigma}_{O_1, 3/0} \right) \cdot \vec{y}_1' = C_{m_1} \quad \text{car } \vec{\sigma}_{O_1, 1/0} = \vec{0}$$

Q.11:

$$C_{m_2} = B_2 \ddot{\theta}_2 + (C_2 - A_2) \sin \theta_2 \cos \theta_2 \omega^2 = D_2$$

$$C_{m_3} = B_3 \ddot{\theta}_3 + (C_3 - A_3) \sin \theta_3 \cos \theta_3 \omega^2 = D_5$$

$$\text{et } C_{m_1} = D_3 + D_6 ; C_{m_2} = D_2 ; C_{m_3} = D_5$$

Q.12: l'équation $C_{m_1} = D_3 + D_6$ reste identique.

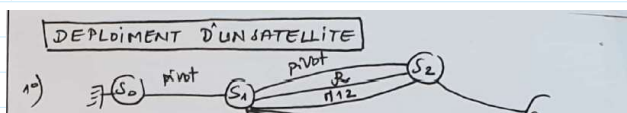
$$C_{m_2} = D_2 + k \theta_2 + \gamma \dot{\theta}_2 \quad \text{et} \quad C_{m_3} = D_3 + k \theta_3 + \gamma \dot{\theta}_3$$

Q.13: Si on isole un des bras, les inconnues de liaison de $S_1 \rightarrow S_2$ vont développer une puissance extérieure. Cette puissance est, pour le bras 2

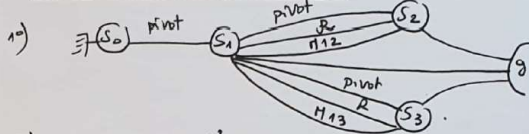
$$S_{\text{ext } S_1 \rightarrow S_2} = \vec{V}_{O_2, 2/0} \cdot \vec{R}_{1/2} + \vec{\Omega}_{2/0} \cdot \vec{H}_{O_2} \text{ de } S_1 \rightarrow S_2$$

Donc on ne peut isoler que le système entier $S_1 + S_2 + S_3$

Q.14:



DEPLOIEMENT D'UN SATELLITE



2°) $T(I/R_0) = \frac{1}{2} C_1 \dot{\psi}^2 + T(S_2/R_0) + T(S_3/R_0)$

$\frac{1}{2} \{ v(S_2/R_0) \} \cdot \{ \theta(S_2/R_0) \}$

$\frac{1}{2} \left\{ \begin{matrix} \vec{v}(z_1) \\ \vec{v}(G_2) \end{matrix} \right\} \cdot \left\{ \begin{matrix} m_2 \vec{v}(G_2) \\ \vec{\sigma}(G_2, z_1) \end{matrix} \right\}_{G_2}$

$\vec{v}(z_1) = \dot{\psi} \vec{z}_0 + \dot{\theta}_2 \vec{y}_1 = \dot{\theta}_2 \vec{y}_2 + \dot{\psi} (\cos \theta_2 \vec{z}_2 - \sin \theta_2 \vec{x}_2)$

$\vec{v}(G_2) = \frac{d}{dt} (v \vec{G}_2)_{R_0} = b_2 \dot{\theta}_2 \vec{x}_2 + (a_2 + b_2 \sin \theta_2) \dot{\psi} \vec{y}_1$

$\vec{\sigma}(G_2, z_1) = \begin{pmatrix} A_2 & 0 & 0 \\ 0 & B_2 & 0 \\ 0 & 0 & C_2 \end{pmatrix}_{R_2} \cdot \begin{pmatrix} -\dot{\psi} \sin \theta_2 \\ \dot{\theta}_2 \\ \dot{\psi} \cos \theta_2 \end{pmatrix}_{R_2}$

$= -A_2 \dot{\psi} \sin \theta_2 \vec{x}_2 + B_2 \dot{\theta}_2 \vec{y}_2 + C_2 \dot{\psi} \cos \theta_2 \vec{z}_2$

$\vec{\sigma}(G_2, z_1) \cdot \vec{v}(z_1) = B_2 \dot{\theta}_2^2 + (A_2 \sin^2 \theta_2 + C_2 \cos^2 \theta_2) \dot{\psi}^2$

$T(z_1/R_0) = \frac{m_2}{2} [(a_2 + b_2 \sin \theta_2)^2 \dot{\psi}^2 + b_2^2 \dot{\theta}_2^2] +$

$\frac{1}{2} [B_2 \dot{\theta}_2^2 + (A_2 \sin^2 \theta_2 + C_2 \cos^2 \theta_2) \dot{\psi}^2]$

et $T(z_3/R_0) = \frac{m_3}{2} [(A_3 + b_3 \sin \theta_3)^2 \dot{\psi}^2 + b_3^2 \dot{\theta}_3^2] + \frac{1}{2} [B_3 \dot{\theta}_3^2 + (A_3 \sin^2 \theta_3 + C_3 \cos^2 \theta_3) \dot{\psi}^2]$

d'où: $T(I/R_0) = \frac{1}{2} C_1 \dot{\psi}^2 + T(2/R_0) + T(3/R_0)$

3°) $P(I \rightarrow I/R_0) = P(S_0 \xrightarrow{Piv} S_1/R_0) + P(G \rightarrow I/R_0)$

$-\frac{d}{dt} v(G \rightarrow I/R_0) \cdot$
 $-\underbrace{m_2 \vec{g} \cdot \vec{O}_1 G_2 - m_3 \vec{g} \cdot \vec{O}_1 G_3}_{m_2 g b_2 \cos \theta_2 + m_3 g b_3 \cos \theta_3}$

$P(I \rightarrow I/R_0) = g [m_2 b_2 \sin \theta_2 + m_3 b_3 \sin \theta_3]$

4°) $P_{int} = -v \dot{\theta}_2^2 + C m_2 \dot{\theta}_2 - k_2 \theta_2 \dot{\theta}_2 - v \dot{\theta}_3^2 + C m_3 \dot{\theta}_3 - k_3 \theta_3 \dot{\theta}_3$

5°) $\frac{d}{dt} T(I/R_0) = P_{ext} + P_{int}$